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Applicant: Oki Electric Industry Company, Limited 7-12, Toranomon 1-chome Minato-ku Tokyo 105(JP)

Inventor: Kikuchi, Hiroshi Oki Electric Industry Co., Ltd.
7-12 Toranomon 1-chome
Minatoku Tokyo(JP)
Inventor: Tanuma Jiro Oki Electric Industry
Co., Ltd.
7-12 Toranomon 1-chome
Minatoku Tokyo(JP)
Inventor: Kasai, Tadashi Oki Electric Industry
Co., Ltd.
7-12 Toranomon 1-chome
Minatoku Tokyo(JP)
Inventor: Ishikawa, Masayuki Oki Electric
Industry Co., Ltd.
7-12 Toranomon 1-chome

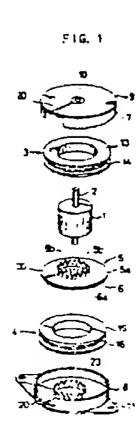
Representative: Read. Matthew Charles et ai Venner Shipley & Co. 368 City Road London EC1V 2QA(GB)

Minatoku Tokyo(JP)

Pulse motor.

In a pulse motor comprising a rotor, a drive coil excited by a predetermined drive current to drive the rotor, and a yoke for guiding a magnetic flux generated by the drive coil to a predetermined magnetic path; the yoke is provided with a through-hole to restrict the flow path of an eddy current induced by the magnetic flux generated by the drive coil.

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PULSE MOTOR

BACKGROUND OF THE INVENTION

The present invention relates to a pulse motor frequently used in printers and the like.

In printers, for example, a pulse motor (stepping motor) having a good controllability is often employed for scanning a print head, or driving a platen roll.

Fig. 2 shows an exploded oblique view of a prior-art pulse motor using a permanent magnet for the rotor

The rotor 1 of this pulse motor comprises a permanent magnet divided and magnetized along its circumference. A rotor shaft 2 is fixed to the center of the rotor 1 by means of a collar, not shown. Provided to surround the rotor 1 are a pair of drive coils 3 and 4, and inner yokes 5 and 6 are disposed between the drive coils 3 and 4. Provided to surround the drive coils 3 and 4 are outer yokes 7 and 8. A flange 9 and a mounting plate 11 are provided at the top and at the bottom. The flange 9 is provided with a bearing 10 for accepting and supporting the rotor shaft 2. The mounting plate 11 is provided with a similar bearing, although not illustrated as such.

The two inner yokes 5 and 6 comprise annular magnetic plates 5a and 6a, respectively, and are provided, at their inner peripheries, n/4 (n being the number of steps per rotation of the rotor) magnetic poles 5b and 6b, respectively, formed by bending so that they are parallel with the rotor shaft 2. In the drawings, the magnetic poles 5b of the inner yoke 5 are shown to be bent upward. The magnetic poles 6b of the inner yoke 6 are bent downward. The magnetic poles 5b of the inner yoke 5 and the magnetic poles 6b of the inner yoke 6 arranged so that their phases are 90° offset relative to each other.

Magnetic poles of the same shape are provided in the same number on the lower surface of the outer yoke 7 and the upper surface of the outer yoke 8. Magnetic poles, not shown, on the outer yoke 7 are provided to confront the magnetic poles 5b on the inner yoke 5 so that their phases are 180° offset relative to each other. Similarly, the magnetic poles 23 on the outer yoke 8 are provided to confront the magnetic poles 6b on the inner yoke 6 so that their phases are 180° offset relative to each other. The drive coils 3 and 4 are of such a configuration that the coil 14 or 16 are wound on the bobbins 13 and 15.

The outer yoke 7, the flange 9, and the outer yoke 8 and the mounting plate 11 are secured by spot wesding or the like. The inner yokes 5 and 6 and the outer yokes 7 and 8 are stacked so as to

surround the rotor 1, and the outer yokes 7 and 8 are fitted over the bobbins 13 and 15. The assembly is thus completed.

In the pulse motor of the above construction, when predetermined alternating currents with their phases offset relative to each other are supplied to the drive coils 3 and 4, the rotor 1 rotates at the corresponding period. The magnetic flux generated by the drive coil 3 passes through the magnetic poles 5b of the inner yoke 5, passes from the central portion of the inner yoke 5 to the outer portion, and passes through the outer periphery of the outer yoke 7, and then through the top surface toward the bearing 10, and then through the magnetic poles, not shown, on the lower surface of the outer yoke 7, and then across the air gap, and then enters the rotor 1. The magnetic flux then passes across the air gap and returns to the magnetic poles of the inner yoke 5. A similar magnetic path is formed for the drive coil 4, with the inner yoke 6 and the outer yoke 8 being included in the path.

The rotor 1 is driven in such a direction that the magnetic paths are shortened. By supplying the drive coils 3 and 4, with alternating currents with their phases 90° relative to each other, a continuous drive force of 4 steps per period of the alternating currents are derived and the rotor 1 is thereby rotated.

In recent years, size reduction, cost reduction and improvement in performance are required in connection with the printers and the like, and attendantly the pulse motors used in these equipment are required to be of a smaller size, and a lower cost, and to have a higher torque, and a higher rotational speed.

An attempt to increase the torque without increasing the outer dimension of the motor itself is to use rare earth magnets in place of the conventional ferrite magnets for the rotor 1. But then the low-price feature of the permanent magnet type pulse motor using permanent magnets for the rotor will be lost.

Another attempt to increase the torque is to increase the current flowing through the drive coils up to the rating. But then the problem of heat generation in the pulse motor itself or the drive current occurs. A countermeasure is to provide a heat sink, cooling fans or the like for the pulse motor or the drive circuit to increase the cooling efficiency. This then raises the cost, and the size of the motor and the peripheral circuits. A further attempt was to optimize the parameters, such as coil constants and the drive currents, to maximize the output with the limited outer dimension. But this also has a limitation.

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SUMMARY OF THE INVENTION

An object of the present invention is to provide a pulse motor in which the heat generation of the yoke is prevented and the drive efficiency is increased.

A pulse motor according to the invention comprises: a rotor; a drive coil excited by a predetermined drive current to drive the rotor; and a yoke for guiding a magnetic flux generated by the drive coil to a predetermined magnetic path; wherein the yoke is provided with a through-hole to restrict the flow path of an eddy current induced by the magnetic flux generated by said drive coil.

In the above pulse motor, the provision of the through-hole in the yoke obstructs to the flow of the eddy current induced by the magnetic flux generated by the drive coil. For instance, a slit intercepting the flow path of the eddy current will reduce the heat generation substantially. If several through-holes are provided in the yoke, being arranged in such a manner as to increase the effective electrical resistance of the flow path for the eddy current, the eddy current can be reduced. The eddy current is reduced in this way, and the heat generation in the yoke is reduced, and the efficiency of the motor can be improved.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is an exploded oblique view showing an embodiment of the pulse motor according to the invention.

Fig. 2 is an exploded oblique view shown a prior-art puise motor.

Fig. 3 is a top view showing an embodiment of an inner yoke used in the motor of the invention.

Fig. 4 is a diagram showing the functions of the eddy current generated in the yoke.

Fig. 5 is a graph showing a torque characteristics of the pulse motor according to the invention.

Fig. 6 is a top view showing a variation of the inner yoke of the motor according to the invention.

Fig. 7 is an exploded oblique view showing the variation of the pulse motor according to the invention.

Fig. 8 is a top view showing another variation of the inner yoke of the motor according to the invention.

DETAILED DESCRIPTION OF THE EMBODI-MENTS

An embodiment of the invention will now be

described with reference to the drawings.

Fig. 1 is an exploded oblique view of an embodiment of a pulse motor according to the invention.

This motor comprises a rotor 1, yokes 5 and 6 surrounding the rotor 1, drive coils 3 and 4, outer yokes 7 and 8, a flange 9 and a mounting plate 11. The construction of the rotor 1, and the drive coils 3 and 4 is the same as that of the prior-art pulse motor described with reference to Fig. 2.

In the pulse motor according to the invention, the inner yokes 5 and 6, and the outer yokes 7 and 8 are each provided with a slit 20 extending radially. The flange 9 and the mounting plate 11 are similarly provided with a slit 20. Except that these slits 20 are provided, the construction of the inner yokes 5 and 6, and the outer yokes 7 and 8 is identical to that of the prior-art pulse motor described with reference to Fig. 2. So the identical parts are denoted by identical reference marks and their description will be omitted. Specific description of the slits 20 will now be given.

Fig. 3 is a top view of an embodiment of the inner yoke 5 used in the motor shown in Fig. 1.

The inner yoke 5 comprises an annular magnetic plate 5a, as was explained earlier, and is provided with a through-hole 17 in the center which permits insertion of the rotor 1. The magnetic poles 5b are arranged around the through-hole 17, at as regular pitch with a predetermined spacing between them. A slit 20 is provided to extend from the through-hole 17 radially up to the outer periphery. The inner yoke 6 shown in Fig. 1 has a similar construction. The slits are formed at an appropriate interval portion between magnetic poles 5b and 6b adjacent to each other, avoiding the magnetic poles necessary for the formation of the magnetic path for the motor drive. Each of the outer yokes 7 and 8 has a similar slit.

The reason why a slit-shaped through-hole is provided in each yoke is as follows:

Fig. 4 is a diagram for explaining the functions of the eddy current generally generated in the yoke 5.

For instance, the drive coil 3 is provided co-axially with and above the yoke 5. The drive coil 3 is supplied with an exciting current in the direction of the arrow 31. The exciting current 31 is an alternating current. The magnetic flux which penetrates the yoke 5 alternates at the same period as the period of the alternating current. As a result, an eddy current is generated in the yoke 5 in the direction of the arrow 32. The yoke 5 is formed of a magnetic material, and has a certain electrical conductivity, so it provides a short-circuiting path for the eddy current 32. As a result, a relatively large current flows and the yoke 5 is heated. Although eddy currents along minor loops are also formed

but they are negligible compared with the eddy current 32.

When a slit 20 is provided to intercept the flow path for the eddy current as shown in Fig. 3, the heat generation can be reduced. When a pulse motor is driven at a high speed, the drive current is an alternating current of a high frequency. Since the eddy current loss is proportional to the square of the frequency, the prevention of the eddy current as described above is effective in prevention of the heat generation and improvement of the efficiency.

Fig. 5 is a graph showing, in comparison, the total torque characteristics of the pulse motor according to the invention and of the prior art. In this graph, the horizontal axis represents the number of drive pulses for the pulse motor (the unit is the number of pulses per second), and the vertical axis represents the crive torque (the unit is gecm). The solid line indicates the torque characteristics of the pulse motor according to the invention, while the broken line indicates the torque characteristics of the pulse motor of the prior art as shown in Fig. 2.

It will be clear from this graph that although there is no substantial difference in the low-speed region, in the high-speed region, in particular, a higher torque can be maintained if the slit is provided than if no slit is provided.

The present invention is not limited to the above embodiment.

Fig. 6 is a top view showing a variation of the inner yoke used in the pulse motor according to the invention. This inner yoke 5 is provided with a number of through-holes 21 elongated in a radial direction. The elongated through-holes 21 also have the function of raising the electrical resistance and restraining the eddy current in the circumferential direction.

This embodiment has an advantage over the embodiment shown in Fig. 3 in that the mechanical strength along the circumferential direction is higher. That is, the inner yoke 5 of the embodiment shown in Fig. 3 must have a sufficient rigidity: otherwise it may be deformed when a twisting force is applied to the inner yoke 5. Moreover, when a force to vary the width of the slit 20 is applied, the positions of the magnetic poles 5b and 6b are changed, and the accuracy of the air gap between the magnetic poles 5b and 6b and the rotor 1 may be lowered. The embodiment shown in Fig. 6 is free from such problems.

Fig. 7 is an exploded oblique view of a variation of a pulse motor employing such an annular yoke. In this embodiment, only the inner yokes 5 and 6, and the outer yokes 7 and 8 are provided with the through-holes 21 and the flange 9 and the mounting plate 11 are not provided with such through-holes. This has an aim of the reinforce-

ment and prevention of entry of dusts into the motor interior.

Fig. 8 is a top view showing another variation of the inner yoke. In this inner yoke 5, a number of circular through-holes arranged in the same direction are provided in place of the elongated through-holes shown in Fig. 6. The effect of increasing the electrical resistance against the eddy current trying to flow in the direction of the circumference can also be increased and the eddy current can be restrained. The yoke with a number of circular through-holes has a higher mechanical strength than the yoke with elongated through-holes.

In a modification, the slit 20 shown in Fig. 3 may have its inner extremity or its outer extremity joined together. In another modification, an insulator or the like is inserted in the slit 20, and bonded with an adhesive to enhance the mechanical strength.

According to the pulse motor of the present invention as described above, when an eddy current is induced in the yoke due to a magnetic flux generated by the drive coil, the eddy current can be effectively restrained, and the eddy current loss is lowered and the drive efficiency of the motor is improved. Moreover, the heat generation due to the eddy current can be prevented and a high-sped drive with a larger current can be achieved without increasing the outer dimension of the motor.

Claims

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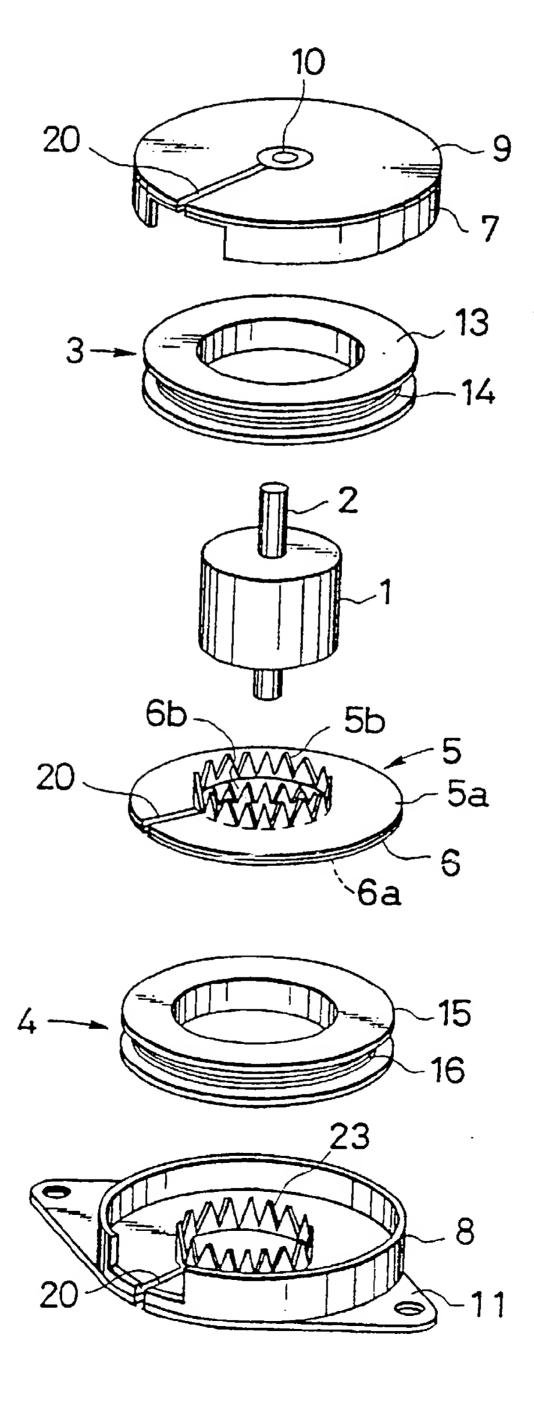
- A pulse motor comprising: a rotor;
- a drive coil excited by a predetermined drive current to drive the rotor; and
- a yoke for guiding a magnetic flux generated by the drive coil to a predetermined magnetic path;
- wherein the yoke is provided with a throughhole to restrict the flow path of an eddy current induced by the magnetic flux generated by said drive coil.
- 2. A pulse motor according to claim 1, wherein said through-hole intercepts the flow path for the eddy current.
- 3. A pulse motor according to claim 1, wherein said through-hole comprises circular perforations arranged in rows in the direction crossing the flow path of said eddy current.
- 4. A pulse motor according to claim 1, wherein said through-hole comprises an elongated hole extending in the direction crossing the flow path of said eddy current.
- 5. A pulse motor according to claim 1, wherein said through-hole is formed at an appropriate interval portion between adjacent magnetic poles to avoid interception of the magnetic path for the

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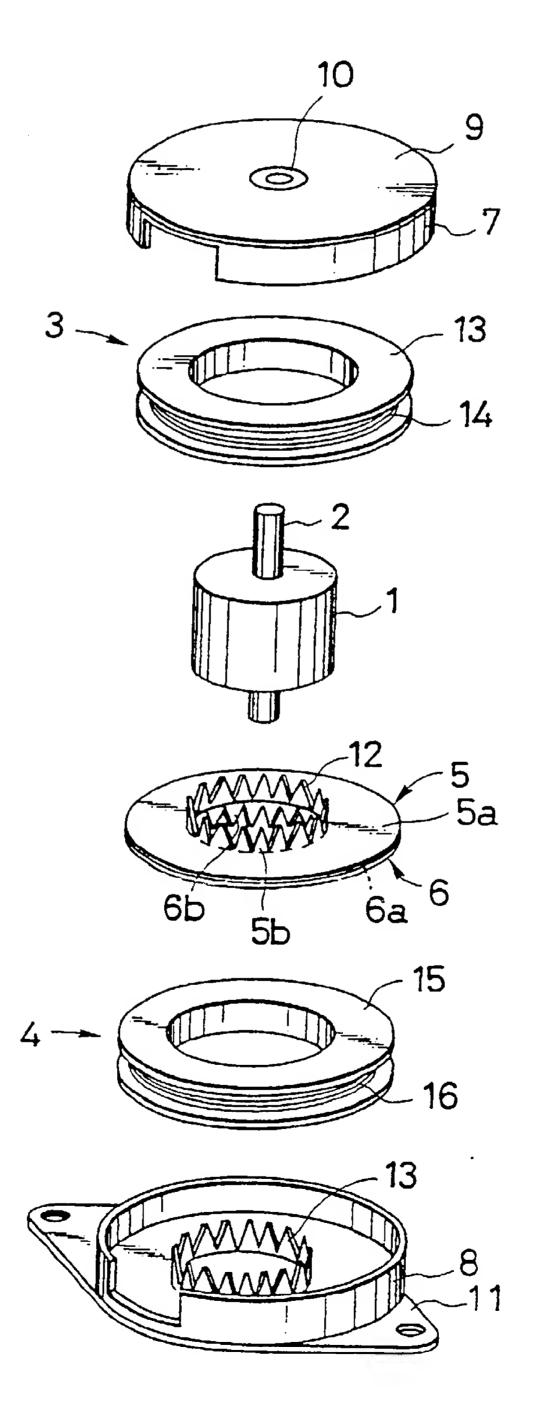
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magnetic flux passing through the magnetic poles necessary for the motor drive.

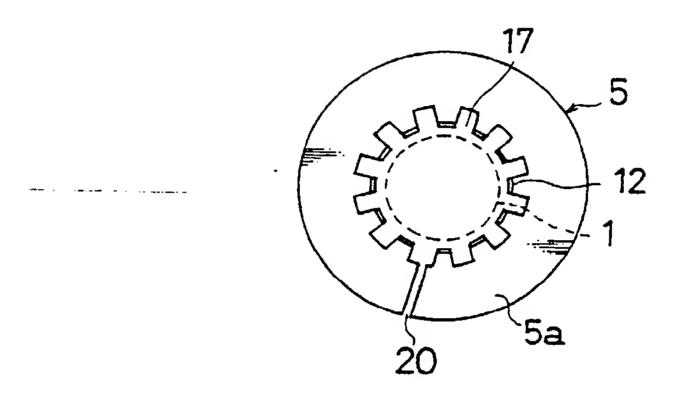
FIG. 1



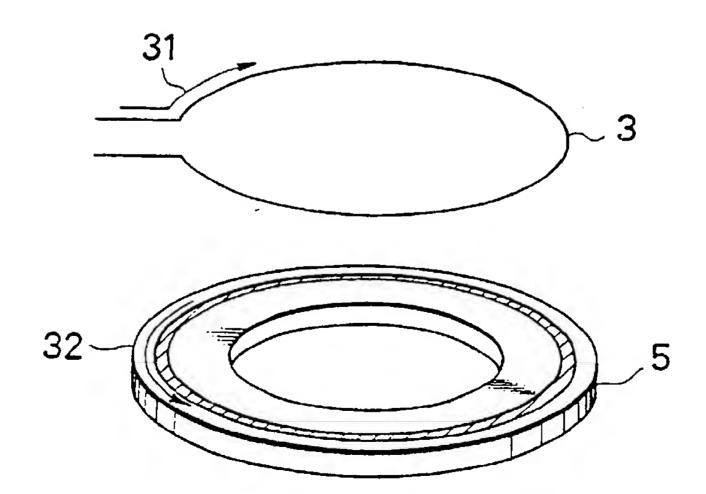
F I G. 2



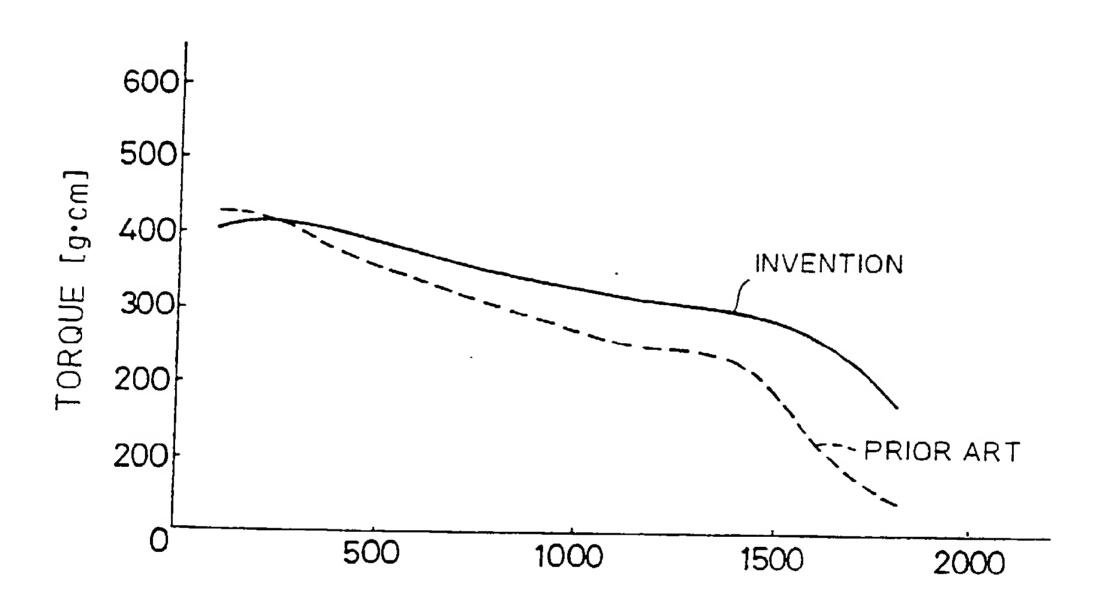
F1G.3



F1G. 4

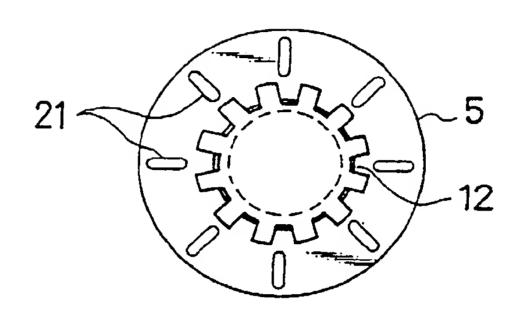


F1G. 5

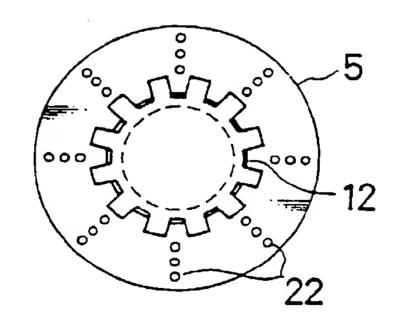


DRIVE PULSE NUMBER PER SECOND [pps]

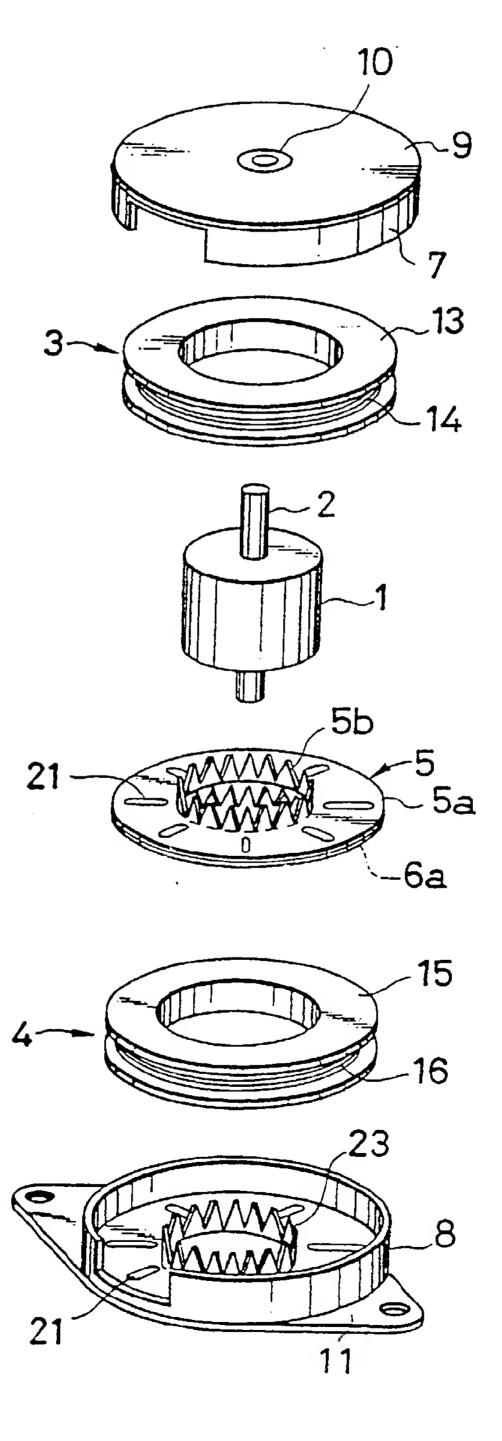
F1G. 6



F1G. 8



F1G. 7





EUROPEAN SEARCH REPORT

Application Number

EP 89 30 4253

Category	DOCUMENTS CONSIDERED TO BE RELEVANT Citation of document with indication, where appropriate, Relevant			
	of relevant passages	ion, where appropriate,	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 4)
X Y	FR-A-2 570 228 (CENTRE * Page 5, line 12 - pag figures 1-3 *	NATIONAL) ge 8, line 24;	1,2,4,5	H 02 K 37/14 H 02 K 21/14 H 02 K 1/14
	IBM TECHNICAL DISCLOSUR 30, no. 1, June 1987, p Armonk, New York, US; "step motor having reductorrents" * Page 375; figures 1,2	ages 374,375, Permanent magnet ed eddy	1,2,4	
Y	IDEM		3	
1	US-A-2 171 988 (POOLE) * Page 4, right-hand column, lines 56-66; figures 7,8 *		1,2	
Y	· 		4,5	
Y (JS-A-4 012 652 (GILBER * Column 3, lines 25-30;	Γ) figures 2,5 *	4,5	TECHNICAL FIELDS
				SEARCHED (Int. Cl.4)
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